

CEMENTING COMPOSITIONS AND APPLICATION OF SUCH
COMPOSITIONS FOR CEMENTING OIL WELLS OR THE LIKE

The present invention relates to techniques for
drilling oil, gas, water, or geothermal wells or the
5 like. More precisely, the invention relates to cementing
compositions which are particularly suitable for
cementing zones which are subjected to extreme static or
dynamic stresses.

In general, a well which is over a few hundred
10 meters deep is cased and the annular space between the
underground formation and the casing is cemented over all
or part of its depth. Cementing essentially prevents the
exchange of fluid between the different layers of
formation traversed by the hole and controls the ingress
15 of fluid into the well, and in particular limits the
ingress of water. In production zones, the casing - and
the cement and the formation - are perforated over a
height of several centimeters.

The cement placed in the annular space of an oil
20 well is subjected to a number of stresses throughout the
lifetime of the well. The pressure inside a casing can
increase or decrease because the fluid which fills it can
change or because additional pressure is applied to the
well, for example when the drilling fluid is replaced by
25 a completion fluid, or during a stimulation operation. A
change in temperature also creates stress in the cement,
at least during the transition period before the steel
and the cement reach temperature equilibrium. In the
majority of the above cases, the stress process is
30 sufficiently slow for it to be treated as a static
process; and in some cases the forces can be sufficiently
large to damage the casing. The cement is also subjected
to other stresses which are dynamic in nature, either
because they are produced over a very short period or
35 because they are either periodic or repetitive in nature.
Perforating creates an over-pressure of several hundred
bars inside a well which is dissipated in the form of a

shock wave. Further, perforating creates a shock when the projectile penetrates the cement and that shock subjects the zone surrounding the hole to large forces over a depth of several meters.

5 A further process, which is now routine in oil well operations and which creates dynamic stresses in the cement, is the opening of a window in a casing which is already cemented to create a multi-branch lateral well. Milling the steel over a depth of several meters followed
10 by drilling a lateral well subjects the cement to shocks and vibrations which usually damage it irreparably.

The present invention aims to provide novel formulations, in particular for cementing regions of oil wells or the like which are subjected to extreme static
15 or dynamic stresses.

An article presented at the SPE (Society of Petroleum Engineers) annual technical conference and exhibition of 1997, Marc Thiercelin et al. (SPE 38598, 5-8 October 1997) - and French patent application
20 FR-A-97 11821 of 23rd September 1997 - demonstrate that the risk of rupture of a cement sleeve depends on the thermoelastic properties of the casing, of the cement, and of the formation surrounding the well. A detailed analysis of the mechanisms leading to rupture of the
25 cement sleeve has shown that the risk of rupture of a cement sleeve following an increase in pressure and/or temperature in the well is directly linked to the tensile strength of the cement and is attenuated when the ratio of the tensile strength R_T of the cement to its Young's
30 modulus E is increased.

Young's modulus is known to characterize the flexibility of a material. To increase that R_T/E ratio, it is advantageous to select materials with a low Young's modulus, in other words to select very flexible
35 materials.

One known means for increasing the flexibility of a hardened cement is to reduce the density of the slurry by

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properties of hardened cements, in particular to improve their elasticity and ductility.

In its French patent application number FR-A-98 16104 dated 21st December 1998, the Applicant
5 describes lightened oil cements reinforced with flexible particles, of low compressibility, with low density, and with an average particle size not exceeding
500 micrometers (μm). The density of the flexible particles is less than 1.5 grams per cubic meter (g/cm^3),
10 preferably less than 1.2 g/cm^3 and more preferably less than 1 g/cm^3 . That results in lightened cement slurries. All of the examples given in French patent application FR-A-98 16104 correspond to a slurry with a density of less than 1.68 g/cm^3 .

15 Further, in patent application FR-A-98 12538, the Applicant also describes cement slurries with a density of less than 1.70 g/cm^3 comprising 30% to 100% (by weight of cement) of rubber particles, with a grain size of 40-60 mesh with a diameter which is preferably in the range
20 250 μm to 400 μm .

As indicated above, a reduction in slurry density tends to encourage its flexibility and is thus usually desired. However, low density may not be desirable in particular when the pressure is high due to the formation
25 or to the nature of other fluids pumped downstream or upstream of the lightened slurry.

The authors of the present invention have set themselves the target of producing cementing slurries reinforced by flexible or rubber particles with a low
30 density, but with the density of the slurries themselves being normal for cementing slurries for oil wells or the like, i.e., typically in the range 1.7 g/cm^3 to 2.2 g/cm^3 .

According to the invention, the problem is solved by cementing slurries for an oil well or the like comprising
35 an hydraulic binder, dense particles with a density higher than the density of the hydraulic binder and reinforcing particles with a density of less than 1.5

g/cm³, preferably less than 1.2 g/cm³, constituted by a rubber or a flexible material, of low compressibility and with an average grain size of less than 600 micrometers (μ m).

5 The flexible particles are constituted by a material with a Young's modulus of less than 5000 mega Pascals (MPa) (preferably less than 3000 MPa, more preferably less than 2000 MPa), i.e., the elasticity of these particles is at least four times greater than that of
10 cement and more than thirteen times that of the silica usually used as an additive in oil well cements. The flexible particles added to the cementing compositions of the invention are also remarkable because of their low compressibility. Materials which are more compressible
15 than rubber, in particular with a Poisson ratio of less than 0.45, preferably less than 0.4, are preferred. However, materials which are too compressible, with a Poisson ratio of less than 0.3, are not preferred.

 Preferred dense particles are particles with a
20 specific gravity of well over 3, such as haematite particles which have a density of 4.95 g/cm³.

 The dense particles and reinforcing particles must be insoluble in an aqueous medium which may be saline, and they must be capable of resisting a hot basic medium
25 since the pH of a cementing slurry is generally close to 13 and the temperature in a well is routinely higher than 100°C.

 Regarding the size of the rubber or flexible particles, essentially isotropic particles are preferred.
30 Spherical or near spherical particles may be synthesized directly, but usually the particles are obtained by grinding, in particular cryo-grinding. The average particle size is generally in the range 80 μ m to 600 μ m, preferably in the range 100 μ m to 500 μ m. Particles
35 which are too fine, also particles which are too coarse, are difficult to incorporate into the mixture or result

in pasty slurries which are unsuitable for use in an oil well.

Particular examples of materials which satisfy the various criteria cited above are thermoplastics
5 (polyamide, polypropylene, polyethylene,...) or other polymers such as styrene divinylbenzene or styrene butadiene (SBR).

In addition to flexible particles and dense particles, the cementing compositions of the invention
10 comprise an hydraulic binder, in general based on Portland cement and water. Depending on the specifications regarding the conditions for use, the cementing compositions can also be optimized by adding additives which are common to the majority of cementing
15 compositions, such as suspension agents, dispersing agents, anti-foaming agents, expansion agents (for example magnesium oxide or a mixture of magnesium and calcium oxides), fine particles, fluid loss control agents, gas migration control agents, retarders or
20 setting accelerators.

A typical composition of the invention comprise, by volume, 2% to 15% of dense particles, 5% to 20% of flexible particles, 20% to 45% of cement and 40% to 50% of mixing water.

25 The formulations of the invention are preferably based on Portland cements in classes A, B, C, G and H as defined in Section 10 of the American Petroleum Institute's (API) standards. Classes G and H Portland cements are particularly preferred but other cements
30 which are known in this art can also be used to advantage. For low-temperature applications, aluminous cements and Portland/plaster mixtures (for deepwater wells, for example) or cement/silica mixtures (for wells where the temperature exceeds 120°C, for example) can be
35 used, or cements obtained by mixing a Portland cement, slurry cements and/or fly ash.

The water used to constitute the slurry is preferably water with a low mineral content such as tap water. Other types of water, such as seawater, can possibly be used but this is generally not preferable.

5 These particles with low density with respect to the cement can affect the flexibility of the system, since adding flexible particles produces cements with a lower Young's modulus, while producing low permeability and better impact resistance.

10 The mechanical properties of the compositions comprising flexible particles of the invention are remarkable, rendering them particularly suitable for cementing in areas of an oil well which are subjected to extreme stresses, such as perforation zones, junctions
15 for branches of a lateral well or plug formation.

The following examples illustrate the present invention.

Cement slurry formulations

Slurries were prepared based on an HMR cement
20 resistant to magnesium salts and based on a Portland cement, furnace clinker and fly ash, polypropylene particles, haematite particles, water and different conventional additives such as a dispersing agent, a retarder and an anti-foaming agent.

25 The formulations and properties of the cement slurries are given in Tables 1 to 3; the density ρ of the cement slurry was about 1.92 g/cm^3 - (16 pounds per gallon - ppg) for all of the compositions. This illustrates a major characteristic of the invention which dissociates
30 the density of the slurry from the flexible particle concentration.

ICO Polymer produced the polypropylene used in this example under the trade name ICORENE 9013 P. Its density was 0.905 g/cm^3 . Its initial specification as regards
35 grain size was such that the grain size of at most 5% of the particles is more than $800 \mu\text{m}$, 30% with a grain size

The average dimension of the haematite particles was 50 μm .

10 The dispersing agent used was a polynaphthalene
sulphonate; the retarder was a lignosulphonate. The
expansion agent was magnesium oxide.

For the solid additives (the expansion agent and the fluid loss control agent), the proportions shown are with respect to the weight of HMR cement (abbreviated to bwoc, "by weight of cement"). For additives in the liquid form (anti-foaming agent, dispersing agent and retarder), the proportions are shown in gallons per sack (gps), i.e., 3.78541 liters per sack of 42.637 kilogram (kg) of HMR cement, in other words 1 gps = 0.0888 liters (l) of additive per kg of HMR cement.

	Haematite		Poly-propylene		Expansion agent	Fluid loss control agent	Anti-foaming agent	Dispersing agent	Retarder
	%bwoc	%bvob	%bwoc	%bvob					
#1	11	5	6	15	2.34		0.038	0.33	0.11
#2	50	16.14	15.2	27	3.30		0.054	0.155	0.155
#3	100	23.54	27	35	4.54	0.45	0.075	0.213	0.213
#4	50	16.14	15.2	27	2.15	0.33	0.054	0.155	0.116

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#2	50	16.14	15.2	27	3.30		0.054	0.155	0.155
#3	100	23.54	27	35	4.54	0.45	0.075	0.213	0.213
#4	50	16.14	15.2	27	2.15	0.33	0.054	0.155	0.116

TABLE 2: Slurry density and porosity

Formulation	Density		Porosity
	ppg	g/cm ³	
#1	16.16	1.936	46%
#2	16.17	1.938	46%
#3	16.22	1.944	46%
#4	16.11	1.930	46%

The rheology of slurries #1 and #4 was measured using the procedure recommended in API 10 (American Petroleum Institute). At laboratory temperature, the rheology was measured immediately after mixing and after 20 minutes of conditioning to temperature. The results are shown in Table 3. The rheology of a slurry was characterized by its plastic viscosity PV (in cP or mPa.s), the conversion factor being equal to 1) and the yield point or Ty (in lbf/100ft², conversion to Pascals being obtained by multiplying by 0.478803), assuming the slurry to be a Bingham fluid.

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TABLE 3: Rheology

Formulation	Rheology after mixing at laboratory temperature		Rheology after conditioning at 85°C	
	PV	Ty	PV	Ty
	(mPa.s)	Ty(lbf/100ft ²)	(mPa.s)	Ty(lbf/100ft ²)
#1	226	9.3	86	9.4
#2	117	6.2	42.6	6.8
#3	131	8.5	68.5	9.1
#4	198	12	131	19.7

These rheology measurements show that the slurry could be pumped in an oil type well.

For slurry #4, the stability was also checked by determining the density profile of a set cement column under pressure and temperature under static conditions. To this end after preparing, the slurry was cast into a cylindrical mold 20.32 cm high and 2.54 cm in diameter. The slurry was mixed and stirred for 20 minutes at 85°C and cast into the mold which had been pre-heated to the same temperature. The temperature was increased by 2°C per minute to the test temperature (120°C). A pressure of 20.68 MPa was applied and maintained throughout the test (24 hours). At the end of the test, the density at the top and bottom of the column was measured. For slurry #4, a difference of 0.013 g/cm³ was determined between the top and bottom which indicated that the slurry was stable even when it contained a large quantity of haematite.

The development of the compressive strength during setting of the cement was evaluated by UCA (Ultrasonic Cement Analyzer) measurements. These measurements enabled the setting time required to produce a given strength (0.34 MPa - 50 psi and 3.4 MPa = 500 psi) and the compressive strength R_t obtained after a given time (24 and 48 hours) at a pressure of 3000 psi (20.7 MPa) to be determined.

TABLE 4: UCA and setting time at T = 120°C

N°	Setting time at 95°C	Time to 0.34 MPa at T (h :min)	Time to 3.4 MPa at T (h :min)	Compressive strength after 24 hours (MPa)	Compressive strength after 48 hours (MPa)
#4	5:17	7:12	7:30	15	17.8

Mechanical properties - compression

The compressive mechanical properties were measured for certain prepared cement slurries.

The influence of adding haematite particles and flexible particles on the mechanical properties of a set cement was studied using systems which had passed several days under high pressure and temperature in high pressure and high temperature chambers to simulate the conditions encountered in an oil well.

The tests were carried out on cubes with 5 cm (2 inch) sides obtained after three days at 120°C and at 20.7 MPa (3000 psi).

For comparison purposes, an NET system was formulated with no flexible particles and no haematite particles, with a density of 1.941 g/cm³ (16.2 ppg), a porosity of 48%, simply prepared with HMR type cement, an anti-foaming agent (0.04 gps) and a dispersing agent (0.02 gps). The results obtained with formulation C1 described in French patent application FR-A-98 16104 were also repeated, constituted by a mixture of class G cement, 19.4% (by weight of cement) of polypropylene particles, 0.022 gps of a dispersing agent, 0.045 gps of a retarder and 0.030 gps of an anti-foaming agent. The porosity of this formulation was 45% and its density was 1.67 g/cm³. The bending and compression tests were carried out on this formulation after 5 days.

The results are shown in Table 5 where Cs designates the compressive strength and Ec represents the compressive Young's modulus.

TABLE 5: Results of compressive tests with flexible particles.

Formulation	CS (MPa)	Ec (MPa)	CS/Ec (x 1000)	Energy (J)
NET	39.2	9041.6	4.33	10.77
C1	21.6	3977.2	5.49	14.28
#1	35.5	6242.6	5.81	19.00
#2	21.1	2594.1	8.17	19.25
#3	13.4	1177.29	11.38	15.94

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drained before carrying out the mechanical tests which were thus carried out on the moist samples.

For formulation #4, the Poisson ratio of the hardened cement was measured at 0.239 for a density of 1.93 g/cm³. For conventional cements with the same density, the Poisson ratio is between 0.15 and 0.2. This indicates that the compressibility of the cements of the invention is lower. Because of this lower compressibility, the hardened cement can more readily distribute lateral forces or can better distribute forces in response to a compressive stress, which is very favorable to good zone isolation.

Expansion measurements

Linear expansion of cement slurries during setting at a temperature simulating well conditions was measured in an annular expansion mold. This mold was constituted by two concentric rings, respectively with a diameter of 51 mm and 89 mm, placed between two flat disks 22 mm apart. The external ring had longitudinal slits and included two scales located either side of the slit enabling distances to be measured during expansion of the cement. The cement slurry to be studied was poured into the mold, and the mold was then placed in a water bath thermostatted at 95°C. The slurry remained in contact with the water throughout the test.

The expansion results are shown in Table 6.

TABLE 6: Expansion results

	Linear expansion, % after 4 days	Linear expansion, % after 6 days	Linear expansion, % after 11 days
NET	0	0	0
#4	0.29	0.29	0.36

The expansion behavior is of particular interest for preventing the cement from separating from the casing and to prevent it from separating from the formation. This behavior is more significant when the cement is flexible and thus is confined by the rock.

The slurries of the invention thus prove to be well suited to cementing in zones subjected to extreme static or dynamic stresses such as perforation zones, junctions of branches of a multi-branch lateral well or salt zones necessitating large changes in mud pressure.